



**Experimental, Numerical Simulation and
Mathematical Modelling of Vane type Vertical Axis
Wind Turbine**

by

**KADHIM HUSSEIN SUFFER AI-ZAEDY
(1341411033)**

A thesis submitted in fulfillment of the requirements for the degree of
Philosophy in Mechanical Engineering

**School of Manufacturing Engineering
UNIVERSITI MALAYSIA PERLIS**

2016

**THESIS DECLARATION FORM
UNIVERSITI MALAYSIA PERLIS**

DECLARATION OF THESIS

Author's full name: KADHIM HUSSEIN SUFFER AL-ZAEDY

Date of birth: 01/06/1967

Title: EXPERIMENTAL, NUMERICAL SIMULATION AND MATHEMATECAL
MODELLING OF VANE TYPE VERTICAL AXIS WIND TURBINE

Academic Session: 2013/2016

I hereby declare that this thesis becomes the property of Universiti Malaysia Perlis (UniMAP) and to be placed at the library of UniMAP. This thesis is classified as:

- CONFIDENTIAL** (Contains confidential information under the Official Secret Act 1972)
- RESTRICTED** (Contains restricted information as specified by the organization where research was done)
- OPEN ACCESS** I agree that my thesis is to be made immediately available as hard copy or on-line open access (full text)

I, the author, give permission to the UniMAP to reproduce this thesis in whole or in part for the purpose of research or academic exchange only (except during a period of ____ years, if so requested above).

Certified by:

SIGNATURE

A11167138

(NEW IC NO./ PASSPORT NO.)

Date: 13-12-2016

SIGNATURE OF SUPERVISOR

Professor Dr. RYSPEK USUBAMATOV

NAME OF SUPERVISOR

Date: 13-12-2016

ACKNOWLEDGEMENTS

Praise be to Allah, the Most Gracious and the Most Merciful and may His salawat and Salaam always be with Prophet Mohammad (p.b.u.h) and his holy progeny eternally. Thanks to God Almighty for His blesses and strength that He has given to me to finish my research. Uncountable thanks are due to my parents for their more love and blessings. They provide me the strength to go through life and all the challenges it brings forth. I would also like to thank them for their continuous support, patience, encouragement and extra care. I want to express my special thanks to my wife, brothers and sisters for their love and encouragement. Thank you very much for supporting me every step of the way.

Most my gratitude goes to my Supervisor Professor Dr. Ryspek Usubamatov for his patience during the supervision of my work, I would also like to express all my gratitude and thank to my first Co-Supervisor Professor Dr. Ghulam Abdul Quadir, who providing valuable guidance and suggestions on this work. My special thanks also go to second Co-Supervisor, the Dean of School Manufacturing Engineering, Associate Professor Dr Khairul Azwan Bin Ismail for his valuable support. My grateful thanks also go to the Technical Staff of school of Manufacturing Engineering and school of Mechatronic Engineering in University Malaysia Perlis, for supporting me in my experimental work. Finally, I would like to thank all the friends who helped me to complete my research.

TABLE OF CONTENTS

| | PAGE |
|------------------------------------|-------------|
| THESIS DECLARATION | i |
| ACKNOWLEDGMENT | ii |
| TABLE OF CONTENTS | iii |
| LIST OF TABLES | vii |
| LIST OF FIGURES | viii |
| LIST OF ABBREVIATIONS | xv |
| LIST OF SYMBOLS | xvi |
| LIST OF NOMENCLATURE | xviii |
| ABSTRAK | xix |
| ABSTRACT | xx |
| | |
| CHAPTER 1 INTRODUCTION | |
| 1.1. Background | 1 |
| 1.2. Renewable Energy | 2 |
| 1.3. Wind Energy | 3 |
| 1.4. Wind Turbine | 4 |
| 1.5. Problem Statement | 7 |
| 1.6. Research Objectives | 8 |
| 1.7. Research Scope and Limitation | 8 |
| 1.8. Research Contributions | 9 |
| 1.9. Thesis Overview | 10 |

CHAPTER 2 LITERATURE REVUEW

| | | |
|---------|-------------------------------------|----|
| 2.1 | Introduction | 12 |
| 2.2 | Wind Turbine History | 13 |
| 2.3 | Wind Turbine Classifications | 15 |
| 2.3.1 | Horizontal Axis Wind Turbine (HAWT) | 17 |
| 2.3.2 | Vertical Axis Wind Turbine (VAWT) | 20 |
| 2.3.2.1 | Savonius Vertical Axis Wind Turbine | 21 |
| 2.3.2.2 | Darrieus Vertical Axis Wind Turbine | 31 |
| 2.4 | Summary | 42 |

CHAPTER 3 RESEARCH METHODOLOGY

| | | |
|---------|-------------------------------------------------------|----|
| 3.1 | Introduction | 43 |
| 3.1.1 | VVAWT Design Steps | 44 |
| 3.1.2 | Experimental Sequence | 50 |
| 3.1.3 | Numerical Simulation CFD | 51 |
| 3.1.4 | Mathematical Modeling | 52 |
| 3.2 | Experimental Investigation with Generator | 54 |
| 3.2.1 | Block Diagram Representation of the Electrical System | 54 |
| 3.2.2 | Calculation of Experimental Parameters | 56 |
| 3.3 | Numerical Simulation (CFD models) | 57 |
| 3.3.1 | Governing Equations | 60 |
| 3.3.1.1 | Continuity Equation | 60 |
| 3.3.1.2 | Momentum Equation | 60 |
| 3.3.1.3 | Turbulence Closure Model ($k - \omega$) | 60 |
| 3.3.2 | Assumptions | 62 |

| | | |
|---------|------------------------------------------------------------------|----|
| 3.3.3 | Mesh Generation | 63 |
| 3.3.4 | Boundary Conditions | 64 |
| 3.3.5 | Solution of the Problem (Processor) | 65 |
| 3.4 | Analytical Approach | 66 |
| 3.4.1 | Analysis of Shadow Effect for Three Blades VVAWT with Open Vanes | 68 |
| 3.4.1.1 | Beginning of Wind Shadow for Three Blades VVAWT | 68 |
| 3.4.1.2 | Maximum Wind Shadowing $W_{sh(max)}$ for Three Blades VVAWT | 71 |
| 3.4.1.3 | End of Wind Shadowing for Three Blades VVAWT | 73 |
| 3.4.2 | Torque Calculations for Three Blades VVAWT with Open Vanes | 75 |
| 3.4.3 | Analysis of Shadow Effect for Four Blades VVAWT with Open Vanes | 79 |
| 3.4.3.1 | Beginning of Wind Shadow for the Four Blades VVAWT | 80 |
| 3.4.3.2 | Maximum Wind Shadowing for Four Blades VVAWT | 81 |
| 3.4.3.3 | End of Wind Shadowing of Four Blades VVAWT | 82 |
| 3.4.4 | Torque Calculations for the Four Blades VVAWT with Open Vanes | 84 |

CHAPTER 4 RESULTS AND DISCUSSIONS

| | | |
|-------|-------------------------------------|----|
| 4.1 | Introduction | 86 |
| 4.2 | Experimental Set-up | 86 |
| 4.2.1 | Test Models Fabrication and Details | 88 |
| 4.2.2 | Models Support Shaft Test | 88 |
| 4.2.3 | Flat Plate Model Test | 90 |

| | | |
|------------------------------|---------------------------------------------------------------------------|-----|
| 4.2.4 | Single Blade Test with Closed Vanes | 93 |
| 4.2.5 | Single Blade Test with Open Vanes | 96 |
| 4.2.6 | Two Blades with Open Vanes Test | 100 |
| 4.2.7 | Experimental Test Three and Four Blades VVAWT with Fixed Positions | 104 |
| 4.3 | Turbine Electrical Power Test | 108 |
| 4.4 | Numerical Simulation CFD Tests | 115 |
| 4.4.1 | Flat Plate CFD Test | 115 |
| 4.4.2 | Cavity Single Blade with Closed Vanes CFD Test | 117 |
| 4.4.3 | Single Blade with Open Vanes CFD Test | 119 |
| 4.4.4 | Two Blades CFD Test | 125 |
| 4.4.5 | Numerical Simulation for Three and Four Blades VVAWT with Fixed Positions | 128 |
| 4.5 | Mathematical Model Results | 148 |
| | | |
| CHAPTER 5 CONCLUSIONS | | |
| 5.1 | Introduction | 159 |
| 5.2 | Conclusions | 159 |
| 5.3 | Recommendations for the Future Work | 162 |
| | | |
| REFERENCES | | 163 |
| APPENDIX-A | | 168 |
| APPENDIX-B | | 173 |
| LIST OF PUBLICATIONS | | 180 |
| LIST OF AWARDS | | 181 |

LIST OF TABLES

| NO. | | PAGE |
|-----|-------------------------------------------------------------------------------------------------------------------------------------|------|
| 1.1 | Advantages and Disadvantages of (HAWT) | 5 |
| 1.2 | Advantages and Disadvantages of (VAWT) | 6 |
| 2.1 | Comparison of the external and internal flow analysis | 27 |
| 3.1 | Values of constants in the (k- ω) model | 61 |
| 3.2 | Number of mesh for modeled geometries | 64 |
| 4.1 | Drag force test results for support shaft measurement in a wind tunnel | 89 |
| B.1 | Results of coefficient of drag for single blade with open vanes. | 173 |
| B.2 | Results of drag force for two blades with 120° model. | 174 |
| B.3 | Results of drag force for two blades with 90° model. | 175 |
| B.4 | Results of torque and total torque for four blades VVAWT. | 176 |
| B.5 | Results of torque and total torque for three blades VVAWT. | 177 |
| B.6 | CFD results of the frontal area for three and four blades VVAWT. | 178 |
| B.7 | Electrical generator power output results with different supplied load and speed of rotation (RPM) for three and four blades VVAWT. | 178 |
| B.8 | Experimental test results of four blades VVAWT with the electrical generator | 179 |
| B.9 | Experimental test results of three blades VVAWT with the electrical generator | 179 |

LIST OF FIGURES

| NO. | | PAGE |
|------|-----------------------------------------------------------------------------------------------------------------------------------------------|------|
| 2.1 | Global-installed wind capacity (1996-2014) | 13 |
| 2.2 | The first windmills in Persia with the image of the windmill structure | 14 |
| 2.3 | (a) Dutch Windmill, (b) Charles Brush wind turbine, Cleveland | 14 |
| 2.4 | Velocities and forces at a section of a rotating HAWT blade. | 15 |
| 2.5 | Wind Turbine classifications | 16 |
| 2.6 | Propeller HAWT types | 17 |
| 2.7 | PIV test bench | 18 |
| 2.8 | Wind turbine meshing | 19 |
| 2.9 | The meshed airfoil geometry | 20 |
| 2.10 | Five bladed vertical axis vane type rotor | 22 |
| 2.11 | The unstructured triangular grid used for the savonius VAWT simulations | 24 |
| 2.12 | Descriptions of the geometry used to modify the position of the obstacle Left: two-blade rotor; Right: three-blade rotor | 25 |
| 2.13 | Performance of the optimized configuration of power coefficient compared to the conventional Savonius turbine with and without obstacle plate | 26 |
| 2.14 | Three Dimensions and fabricated views of three Savovius rotor models | 28 |
| 2.15 | Velocity distribution at peak performance for three types simulated at TSR | 29 |
| 2.16 | Three types and dimension of tandem blade of Savonius design | 30 |
| 2.17 | Pressure contours for TSR = 3 at different blade angular positions; (a) 90° and (b) 270° | 32 |
| 2.18 | The Preferred Energy (PE) 1 kW VAWT design; (a) CAD geometry and (b) completed to ready for in-situ testing | 33 |

| | | |
|------|---------------------------------------------------------------------------------------------------------------------------|----|
| 2.19 | (a) Triangular hub structure and (b) Square hub structure | 35 |
| 2.20 | The 2-dimensions fluid domain of the VAWT studied during the CFD analysis | 36 |
| 2.21 | Straight blade VAWT using NACA0012 airfoil (a) Sliding mesh near the rotor, (b) Contours of absolute velocity for TSR = 4 | 37 |
| 2.22 | Z -vorticity at different angular positions ($\Delta\theta = 30^\circ$) and TSR = 1.52 | 38 |
| 2.23 | Sample 2-D mesh discretization of the VAWT | 39 |
| 2.24 | Sketch of the flat horizontal vane type wind turbine | 40 |
| 3.1 | Designed geometry of flat plate | 45 |
| 3.2 | Designed single blade geometries, (a) closed vanes, (b) opened vanes | 46 |
| 3.3 | Designed two blades geometries having a fixed angle between them; (a) angle 120° , (b) angle 90° | 47 |
| 3.4 | The isometric of designing VVAWT geometries having closed vanes; (a) three blades, (b) four blades | 48 |
| 3.5 | The isometric of designing VVAWT geometries having opened vanes; (a) three blades, (b) four blades | 49 |
| 3.6 | Isometric and three projection views for four blades design with open vanes. | 50 |
| 3.7 | Research methodology flow chart | 53 |
| 3.8 | Flow chart for basic wind turbine electric system. | 54 |
| 3.9 | Wind turbine system, electrical circuit | 55 |
| 3.10 | Computational domain and boundary conditions for three blades model | 59 |
| 3.11 | Top view of computational domain and boundary conditions (a) three blades, (b) four blades | 59 |
| 3.12 | Tetrahedral volume mesh for open vanes three blades model created in Gambit software | 63 |
| 3.13 | Top view for analysis of three blades VVAWT | 67 |
| 3.14 | Beginning of wind shadow for three blades VVAWT | 69 |
| 3.15 | Wind shadow effect for three blades VVAWT | 71 |

| | | |
|------|-------------------------------------------------------------------------------------------------------------------------------------------|----|
| 3.16 | Maximum wind shadow effect for three blades VVAWT | 72 |
| 3.17 | Reduction of wind shadow effect for three blades VVAWT | 73 |
| 3.18 | End of wind shadow effect for three blades VVAWT | 74 |
| 3.19 | The range of wind shadow effect for three blades open vanes VVAWT according to second blade angular position | 75 |
| 3.20 | Initial position for four blades VVAWT with movable vanes | 80 |
| 3.21 | Maximum wind shadow effect for four blades VVAWT | 81 |
| 3.22 | End of wind shadow effect for four blades VVAWT | 82 |
| 3.23 | The range of wind shadow effect for four blades open vanes VVAWT according to second blade angular position | 83 |
| 4.1 | Low speed wind tunnel equipment and measuring tools | 87 |
| 4.2 | Models support shaft test in wind tunnel | 89 |
| 4.3 | Flat plate test in wind tunnel | 90 |
| 4.4 | Drag force versus upstream air flow velocity for flat plate in wind tunnel test at angular position 90° | 92 |
| 4.5 | Drag coefficient versus upstream air flow velocity for flat plate in wind tunnel test | 92 |
| 4.6 | Drag coefficient versus angular position with different upstream air flow velocity for flat plate in wind tunnel test. | 93 |
| 4.7 | Single blade with closed vanes in wind tunnel test section | 94 |
| 4.8 | Drag force versus upstream air flow velocity for single blade with closed vanes in wind tunnel test | 94 |
| 4.9 | Drag coefficient versus upstream air flow velocity for single blade with closed vanes in wind tunnel test | 95 |
| 4.10 | Drag coefficient versus angular position with different upstream air flow velocity for single blade with closed vanes in wind tunnel test | 95 |
| 4.11 | Fabricated single blade with open vanes mounted in the test section of the wind tunnel at 180° angular position | 97 |
| 4.12 | Drag force versus blade angular position for single blade with open vanes in wind tunnel test | 97 |

| | | |
|------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----|
| 4.13 | Drag Coefficient versus upstream air flow velocity for single blade with open vanes in wind tunnel test | 98 |
| 4.14 | Drag coefficient versus blade angular position for single blade with open vanes in wind tunnel test | 98 |
| 4.15 | Comparison of C_D for flat plate and single blade with open and closed vanes at upstream air flow velocity 7 m/s and different angular positions | 99 |
| 4.16 | Fabricated two blades models with open vanes; (a) 120° for three blades rotor, (b) 90° for four blades rotor | 100 |
| 4.17 | Drag force F_{Dsh} for two blades with 120° models having open vanes versus the blade angular positions | 102 |
| 4.18 | Drag force F_{Dsh} for two blades with 90° model having open vanes versus the blade angular positions | 103 |
| 4.19 | Drag Coefficient C_{Dsh} for two blades with 120° models having open vanes versus the blade angular positions | 103 |
| 4.20 | Drag Coefficient C_{Dsh} for two blades with 90° models having open vanes versus the blade angular positions | 104 |
| 4.21 | Fabricated VVAWT models in wind tunnel test. (a) three blades closed vanes, (b) four blades closed vanes, (c) three blades open vanes, and (d) four blades closed vanes | 105 |
| 4.22 | Variation of C_D results obtained from experimental test for three blades model in cases of open and closed vanes with different blade angular positions | 106 |
| 4.23 | Variation of C_D results obtained from experimental test for four blades model in cases of open and closed vanes with different blade angular positions | 106 |
| 4.24 | Comparison of variation of experimental C_D between three and four blades models for closed vanes case with different blade angular positions | 107 |
| 4.25 | Comparison of variation of experimental C_D between three and four blades models for open vanes case with different blade angular positions | 107 |
| 4.26 | Experimental setup photo for testing the turbine models with electrical generator and transmission gear | 108 |
| 4.27 | Number of Revolutions per Minutes (RPM) with upstream air flow velocity test results for three and four blades VVAWT models | 110 |

| | | |
|------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------|-----|
| 4.28 | Generator power output for number of revolutions per minutes (RPM) and different electrical resistances for three and four blades VVAWT models | 111 |
| 4.29 | Variation of generator power output for three and four blades turbine models with upstream air flow velocity | 112 |
| 4.30 | Compression of experimental power coefficient (C_p) between three and four blades turbine models with upstream air flow | 113 |
| 4.31 | Compression of experimental power coefficient (C_p) between three and four blades turbine models with different tip speed ratio | 114 |
| 4.32 | Compression of experimental torque coefficient (C_t) between three and four blades turbine models with different tip speed ratio | 114 |
| 4.33 | Contours of static pressure distributions around the flat plate model | 116 |
| 4.34 | Contours of velocity magnitude distributions around flat plate model, (b) Contours of turbulent kinetic energy (k) distributions around flat plate model | 116 |
| 4.35 | Contours of static pressure distributions for single blade closed vanes | 118 |
| 4.36 | Contours of velocity magnitude distribution around single cavity blade, (b) Contours of turbulent of kinetic energy (k) distribution around single cavity blade | 118 |
| 4.37 | Coefficient of drag C_D for single blade with open vanes at different blade angular positions from CFD and experimental tests | 119 |
| 4.38 | Contours of static pressure distributions around single blade open vanes at different angular positions | 120 |
| 4.39 | Contours of velocity magnitude distributions around single blade open vanes with different angular positions | 122 |
| 4.40 | Contours of turbulent of kinetic energy (k) distributions around single blade open vanes with different angular positions | 124 |
| 4.41 | Contours of static pressure distributions around of (a) two blades with 120° and (b) two blades with 90° | 127 |
| 4.42 | Contours of velocity magnitude distributions around of (a) two blades with 120° and (b) two blades with 90° | 127 |
| 4.43 | Contours of turbulent kinetic energy distributions (k) around of (a) two blades with 120° and (b) two blades with 90° | 128 |

| | | |
|------|---------------------------------------------------------------------------------------------------------------------------------------------------------------|-----|
| 4.44 | Variation of predicted turbine frontal areas with different blade angular positions for three and four blades models for open and closed vanes | 129 |
| 4.45 | Variation of predicted C_D from CFD tests for three blade model with different blade angular positions in cases of open and closed vanes | 130 |
| 4.46 | Variation of predicted C_D from CFD tests for four blade model with different blade angular positions in cases of open and closed vanes | 131 |
| 4.47 | Comparison of coefficient of drag C_D from CFD test with different blade angular positions for three and four blades in case of open vanes | 132 |
| 4.48 | Comparison of coefficient of drag C_D from CFD test with different blade angular positions for three and four blades in case of closed vanes | 132 |
| 4.49 | Contours of static pressure distributions in and around three blades turbine at different angular position, at left closed vanes, right open vanes | 134 |
| 4.50 | Contours of static pressure distribution in and around four blades turbine at different angular positions; left closed vanes, right open vanes | 135 |
| 4.51 | Velocity vectors magnitude distributions in and around three blades turbine; left closed vanes, right open vanes | 137 |
| 4.52 | Velocity vectors magnitude distributions in and around four blades turbine; left closed vanes, right open vanes | 137 |
| 4.53 | Contours of velocity magnitude distributions in and around three blades turbine at different angular positions; left closed vanes, right open vanes | 139 |
| 4.54 | Contours of velocity magnitude distributions in and around four blades turbine at different angular positions; left closed vanes, right open vanes | 140 |
| 4.55 | Contours of turbulent kinetic energy (k) distributions in and around three blades turbine at different angular positions; left closed vanes, right open vanes | 142 |
| 4.56 | Contours of turbulent kinetic energy (k) distributions in and around four blades turbine at different angular positions; left closed vanes, right open vanes | 144 |

| | | |
|------|----------------------------------------------------------------------------------------------------------------------------------------------------------|-----|
| 4.57 | Comparison of variation of C_D between CFD and experimental results for three blades model in open vanes case with different blade angular positions | 146 |
| 4.58 | Comparison of variation of C_D between CFD and experimental results for three blades model in closed vanes case with different blade angular positions | 146 |
| 4.59 | Comparison of variation of C_D between CFD and experimental results for four blades model in open vanes case with different blade angular positions | 147 |
| 4.60 | Comparison of variation of C_D between CFD and experimental results for three blades model in closed vanes case with different blade angular positions | 147 |
| 4.61 | Drag coefficient for three and four blades models in case of open vanes | 149 |
| 4.62 | Total and average torque for three blades VVAWT open vanes | 150 |
| 4.63 | Total and average torque for four blades VVAWT open vanes | 150 |
| 4.64 | Caparison for the total torque for three and four blades open vanes VVAWT with different blades angular position | 151 |
| 4.65 | Number of turbine rotor revolutions per minutes (RPM) for three and four blades turbine models | 152 |
| 4.66 | Three and four blades turbine power coefficient C_p with upstream air flow velocity | 153 |
| 4.67 | Three and four blades turbine power coefficient (C_p) with tip speed ratio | 154 |
| 4.68 | Three and four blades turbine torque coefficient (C_t) with tip speed ratio | 154 |
| 4.69 | Variation of experimental and calculated power coefficient (C_p) for three blades turbine with different upstream air flow velocity | 155 |
| 4.70 | Variation of experimental and calculated power coefficient (C_p) for three blades turbine with different tip speed ratio | 156 |
| 4.71 | Variation of experimental and calculated torque coefficient (C_t) for three blades turbine with different tip speed ratio | 156 |
| 4.72 | Variation of experimental and calculated power coefficient (C_p) for four blades turbine model with different upstream air velocity | 157 |

| | | |
|------|-----------------------------------------------------------------------------------------------------------------------------------|-----|
| 4.73 | Variation of experimental and calculated power coefficient (C_p) for four blades turbine model with different tip speed ratio | 158 |
| 4.74 | Variation of experimental and calculated torque coefficient (C_t) for four blades turbine with different tip speed ratio | 158 |

LIST OF ABBREVIATIONS

| | |
|--------|---------------------------------------------------|
| CFD | Computational fluid dynamics |
| DMST | Multiple streamtube model |
| HAWT | Horizontal axis wind turbine |
| SIMPLE | Semi-Implicit method for pressure-linked equation |
| SST | Shear Stress Transport |
| VAWT | Vertical axis wind turbine |
| VVAWT | Vane type vertical axis wind turbine |

LIST OF SYMBOLS

| | | |
|------------|-----------------------------------------------|-----------|
| A | Area | m^2 |
| A_s | Swept area | m^2 |
| b | Blade arm dimension | m |
| c | Blade width | m |
| C_p | Power coefficient | |
| C_p | Coefficient of pressure | |
| C_t | Torque coefficient | |
| C_D | Coefficient of drag | kg/s |
| C_{Dsh} | Coefficient of drag under wind shadow effect | kg/s |
| D | Turbine diameter or width of the wind turbine | m |
| D_ω | Cross-diffusion term | |
| E | Kinetic energy | m^2/s^2 |
| F_D | Drag force | N |
| F_{Dsh} | Drag force under wind shadow effect | N |
| f | Damping function in pressure strain tensor | |
| G_k | Generation of (k) | |
| G_ω | Generation of (ω) | |
| H | High of the turbine rotor | m |
| k | Turbulent kinetic energy | |
| N | Number of rotation | RPM |
| N_t | Gear box efficiency | |

| | | |
|------------|--------------------------------------------|------------------|
| N_g | Generator efficiency | |
| P | Pressure | N/m ² |
| ΔP | Pressure difference | N/m ² |
| Re | Reynolds number | |
| R_t | Turbulent Reynold number | |
| R | Turbine rotor radius | m |
| S_k | Source term of (k) | |
| S_ω | Source term of (ω) | |
| T | Torque | N.m |
| t | Time | s |
| U | Mean velocity components | m/s |
| \bar{U} | Time- averaged velocity in x_i direction | m/s |
| V | Wind speed | m/s |
| X_i | x - direction | |
| W | power output | W |
| W_e | Power produce by electrical generator | W |
| W_m | Mechanical power output | W |
| W_{sh} | Width of wind shadow | m |
| W_t | Turbine power output | W |
| W_{wind} | Kinetic power produce by wind turbine | W |
| Y_k | Dissipation of (k) | |
| Y_ω | Dissipation of (ω) | |

LIST OF NOMENCLATURE

| | | |
|-----------------|-----------------------------------------------|--------------------|
| β | Angular position between turbine blades | Deg. |
| γ | Angular position for the first blade | Deg. |
| \mathbb{T} | Mass-averaged viscous stress tensor | |
| θ | Angle between frames | Deg. |
| λ | Tip speed ratio | |
| μ | Kinetic viscosity | N.s/m ² |
| μ_t | Turbulent eddy viscosity | N.s/m ² |
| ω | Specific turbulent dissipation rate | |
| ρ | Density | kg/m ³ |
| ω_t | Angular speed of the rotating turbine | rad/s |
| η | Over all wind turbine efficiency | |
| α_o | Initial angular position for the second blade | Deg. |
| α_1 | Angular position for the second blade | Deg. |
| σ_k | Model constant | |
| σ_ω | Model consta | |

Model dan Simulasi Untuk Reka Bentuk Turbin Angin Paksi Menegak

ABSTRAK

Ekonomi global semasa mencadangkan penggunaan tenaga sumber-sumber yang boleh diperbaharui seperti suria, angin dan biomass untuk menghasilkan kuasa yang diperlukan. Tenaga boleh diperbaharui ialah tenaga alternatif yang bersih, tidak toksik, dan mudah didapati. Teknologi berkaitan tenaga angin telah menyaksikan pertumbuhan yang pesat di seluruh dunia. Turbin angin adalah peranti tipikal yang menukar tenaga kinetik angin ke elektrik. Penyelidikan lalu telah membuktikan bahawa turbin angin paksi menegak (VAWT) menghasilkan kuasa yang lebih tinggi daripada turbin angin paksi mendatar (HAWT). Dalam kajian ini, turbin angin paksi menegak, VVAWT dengan dua rotor yang berbeza (tiga atau empat bilah), yang mempunyai bilah-bilah alih, akan dikaji prestasinya. Model akan dibangunkan daripada bahan ringan dan setiap aspek kira untuk memastikan bilah-bilah ini dapat menahan kelajuan tiupan angin. Di samping itu, saiznya ditetapkan mengikut dimensi terowong angin kelajuan rendah yang terdapat di Universiti Malaysia Perlis. Eksperimen dan simulasi dijalankan bagi plat rata untuk mendapatkan pekali seret dan dibandingkan dengan keputusan yang terdapat dalam kajian. Eksperimen dan simulasi dijalankan untuk model bilah tunggal (dengan bilah-bilah tertutup dan terbuka) dan dua bilah (dengan bilah-bilah terbuka sahaja) yang mempunyai sudut berbeza antara bilah-bilah ini untuk mewakili turbin tiga dan empat bilah. Kajian simulasi tiga dimensi dijalankan untuk meramal ciri-ciri aerodinamik bagi model semasa, menggunakan perisian komersil Dinamik Bendalir Komputeran (CFD) - SolidWork2013, GAMBIT dan FLUENT. Dalam tegasan ricih pengangkutan (SST), model pergolakan $k-\omega$ adalah lebih baik daripada model pergolakan lain, seperti yang disarankan oleh beberapa penyelidik. Medan aliran disimulasi pada kelajuan masuk yang tetap. Model matematik dihasilkan untuk mengira keluasan kesan bayang-bayang bilah-bilah turbin ini di bawah kesan bayangan angin supaya diketahui pekali seret untuk tiga dan empat bilah VVAWT yang digunakan untuk pengiraan tork dan kuasa turbin. Untuk tujuan pengiraan tork di bawah kesan bayang-bayang angin, eksperimen dan penyiasatan simulasi dijalankan bagi tiga dan empat bilah VVAWT di kedudukan sudut bilah tetap pada kelajuan aliran udara hulu yang berbeza. Eksperimen juga dijalankan bagi tiga dan empat bilah yang menggunakan transmisi gear dan penjana elektrik untuk mendapatkan output kuasa penjana elektrik. Keputusan ujian digunakan untuk mengesahkan keputusan simulasi dan matematik. Keputusan dibentangkan dalam bentuk pekali seret, bilangan revolusi per minut (RPM). Adalah didapati bahawa nilai bagi turbin empat bilah adalah lebih tinggi daripada turbin tiga bilah bagi halaju aliran udara hulu yang sama. Keputusan juga diberikan dalam bentuk kuasa pekali C_P dan petua λ nisbah kelajuan. Bagi model turbin tiga bilah dengan bilah-bilah yang terbuka, C_P maksimum adalah 0.121 pada 20.6 m/s halaju hulu dan pada λ bersamaan 0.2511. Manakala bagi model turbin empat bilah dengan bilah-bilah terbuka, C_P maksimum adalah 0.237 iaitu 20.6 m/s halaju hulu dan pada λ bersamaan 0.2663. Adalah didapati bahawa turbin empat bilah VVAWT adalah 51% lebih cekap berbanding dengan turbin tiga bilah VVAWT.

Modeling and Numerical Simulation for the Vane Designs Vertical Axis Wind Turbine

ABSTRACT

The present global energy economy suggests the use of renewable sources such as solar, wind and biomass to produce the required power. Renewable energy is an alternative energy, which is a clean, nontoxic energy source that is available in abundance. Technology related to wind energy has seen a rapid growth worldwide. Wind turbines are typical devices that convert the kinetic energy of wind into electricity. Researches in the past have proved that Vertical Axis Wind Turbines (VAWTs) produce higher power than the Horizontal Axis Wind Turbines (HAWTs). In the present work the Vane type Vertical Axis Wind Turbine, VVAWT, with two different rotors (three and four blades) having movable vanes are investigated in terms of performance. The models are made of light material and every care is taken to ensure that the blades withstand high wind velocities. The sizes of the blades are constrained by the dimensions of the low speed wind tunnel available at University Malaysia Perlis. Experimental and numerical works are carried out for a flat plate to obtain its coefficient of drag, and the results are compared to the results available in the literature. Then, experimental and numerical investigations are carried out for three- and four-blade VVAWT at fixed blade angular positions and for different upstream air flow velocities. The three dimensional numerical investigations are carried out to predict the aerodynamics characteristic of the current models, using commercially available computational fluid dynamic (CFD) software - SolidWork2013, GAMBIT and FLUENT. The Shear Stress Transport (SST), $k-\omega$ turbulence model is used, which is better than other turbulence models available, as suggested by some researchers. The flow field is simulated numerically at a fixed inlet velocity. Mathematical models are developed to calculate the shadow area of the turbine blades under the effect of wind shadow to gauge the coefficient of drag for three- and four-blade VVAWT. These are then used in the calculation of torque and the power of the turbine. For torque calculations under wind shadow effect, experimental and numerical works are carried out for models of single blade (with closed and open vanes) and two blades (with open vanes only) having different angles between the blades to represent three- and four-blade VVAWT. Experimental works are also carried out for three and four blades using transmission gear and electrical generator to measure the electrical generator power output. Experimental results are used to validate numerical and mathematical results. The results are presented in the form of a drag coefficient, torque and the number of revolutions per minute (RPM). It is found that the values for the four-blade turbine are higher than that of three-blade turbine for the same upstream air flow velocities. The results are also presented in the form of power coefficient C_P and tip speed ratio λ . It is found that for the three-blade turbine model with open vanes, the maximum C_P is 0.121 at 20.6 m/s upstream air flow velocity and at λ equal to 0.2511. For the four-blade turbine model with open vanes, the maximum C_P is 0.237 at 20.6 m/s upstream air flow velocity and at λ equal to 0.2663. It is found that the four- blade VVAWT is 51 % more efficient than the three-blade VVAWT.

CHAPTER 1

INTRODUCTION

1.1 Background

The basic necessities for sustaining economic development for fast growing population in any country are energy and water. It is expected that by 2050, energy demand may double or even triple because of the global population growth and the expansion of developing countries' economies. Therefore, finding sufficient supplies of clean and sustainable energy for the future is the global society's most daunting challenge for the twenty-first century. It is expected that the future will be a mix of energy technologies with renewable sources such as solar, wind and biomass playing an increasingly important role in the new global energy economy (Foster, et al., 2009). The exploration of all aspects of energy production and consumption, including energy efficiency and clean energy, is urgently required.

Since approximately 200 years ago, the world has begun dependence on fossil fuels. The fossil fuel era expanded with the discovery of oil. Due to high demand of energy, more fossil fuels such as coal are burnt, resulting in CO₂ emission into the atmosphere. The global climate has somewhat changed because of the emission of CO₂ into the atmosphere. This is normally referred to as global warming. Developed nations solve this problem by investing heavily in renewable energy sources. As it is, there are only a few non-renewable energy sources in the world, and the energy from these sources drain very fast due to rapidly growing demands. Alternative energy in the form of

renewable energy has to be found in order to address the energy issues of the future. The world hopes for a sustainable future, and hence a renewable energy revolution is needed. A sustainable future belongs to sources of clean energy and to those who prepare for it right now.

1.2 Renewable Energy

Energy can be divided into two types, namely non-renewable energy and renewable energy. Non-renewable energy does not regenerate itself at a sufficient rate for sustainable economic extraction in the human timescale. Examples of the sources of this type of energy include petroleum, natural gasoline, coal and nuclear energy. Unfortunately, these carry many issues. For example, harnessing nuclear energy is highly risky, while traditional fossil fuels are very quickly depleting. The world needs to find substitutes for these energy sources, which should be pollution free and abundantly available. Therefore, the attention concentrated on non-renewable energy sources has now shifted to renewable energy sources, particularly efficient renewable energy sources.

Renewable energy is energy that comes from sources that are naturally renewing itself on a human timescale. Examples of renewable energy are wind energy, solar energy, tidal energy, geothermal energy, gravitational energy and biomass energy. Renewable energy is an alternative energy that is clean, nontoxic and abundantly available in nature. The strategy of many nations is to supply energy from renewable sources, especially when there are numerous environmental sustainability concerns that must be addressed appropriately (Johnson, 2006).

There are many advantages of using renewable energy, such as sustainability (cannot be depleted), ubiquity (found everywhere across the world in contrast to

fossil fuels and minerals), generally non-polluting and carbon free. Non-renewable energy sources can be acquired from almost all over the world, which is in contrast to fossil fuels and minerals. Non-renewable energy is also environmental friendly as it does not contaminate its surroundings. For wind energy, it does not need water in the production of electricity, and this gives much advantage in dry areas across the world, such as at the southwest and most of the west of the United States of America (Nelson & Starcher, 2015).

However, there are also disadvantages of renewable energy, including its variability, low density, and generally higher initial cost. To add, renewable energy sources may cause visual pollution, odor (from biomass), perceived avian issues (for wind plants), and large land requirements (for solar plants) (Foster et al., 2009).

1.3 Wind Energy

Wind energy has been utilized for at least 3000 years for sailing ships, milling grains and pumping water. Wind is produced because of the uneven solar heating of the earth's land and sea surfaces. The first vertical axis windmill in 644 AD had sails connected to a vertical shaft connected to a grinding stone for milling purposes. In the middle ages, the post-mill was first invented in Europe, and this was independent from the vertical-axis wind wheels of the Orient.

Among all available renewable energy sources, wind energy has the advantage of being available in abundance, clean, and inexhaustible. It has no contribution to global warming, and it requires less installation and maintenance cost for power generation (Foster et al., 2009). With the first oil price shock in the early 1970s, interest in wind power reemerged. Providing electrical energy from the wind has now become important