Figure 3.15: Explode Drawing.

## CHAPTER 4

## RESULTS AND DISCUSSION

### 4.1 Introduction

In order to achieve the result, this chaptecfocused on the result and discussion based on objective which is analytical analysis and simulation by CATIA software. Based on analytical analysis, the result is all about to check each part for it strength, minimum FOS, and maximum displacement. All part of design used ASTM A36 steel as the material on each part of design. The purpose using this material is because less expensive, high strength, sustainable and modifiable. There is several type of strength for material steel such as Table 4.1. According to analytical analysis, there are two parts that will be analyzed which is crank and pin. In addition, the purpose of this analysis is to find their strength of material when applied maximum distributed force.

Table 4.1: Typical Tensile Strength of Some Materials.

| Material | Yield strength <br> (MPa) | Density (g/cm ${ }^{3}$ ) |
| :--- | :--- | :--- |
| Steel, ASTM A36 | 250 | 7.8 |
| Steel, 1090 mild | 247 | 7.58 |
| Steel, 2800 Maraging Steel | 2617 | 8.00 |
| Steel, AerMet 340 | 2160 | 7.86 |


| Steel, high strength alloy ASTM A514 | 690 | 7.8 |
| :--- | :--- | :--- |

Using CATIA software, the simulation is focused on movement of gripper to complete for one cycle with continuously. Each part has different value of properties and produces the different result of Factor of Safety (FOS). FOS is defined as ratio of actual strength of material to design load. Moreover, FOS cannot be greater than 1.0 to prevent from failure occur on structure. FOS will be calculated using equation 4.1.

Factor of Safety, FOS $=\frac{\text { Yield strength }}{\text { Design Load }}$

### 4.2 Animation using CATIA software

Based on simulation that had been figured, gripper and crank selected as main function to make horizontally motion such on Table 4.2. The animation generated by using Digital Mockup Kinematics on CATIA software. Gripper move horizontally and give the different force when the motorstart rotates. The animation show the motion of gripper will be tested without locate a specimen. Based on animation, the value of force is different on each angle on each view of motion gripper.

Table 4.2: Motion of Gripper.

[^0]


### 4.2.1 Kinematic Analysis

Based on animation had been figured, each of angle crank motion will be calculated when machine operated. Each of angles will give different force when gripper starts to pull. The calculation will show about finding force without apply specimen on machine. Figure 4.1 shows free body diagram on how to find force $(\mathrm{P})$ on each angle.


Figure 4.1: Free Body Diagram
Assumption:

Length of rod: 80mm (Specification of design)
Radius of pin: 15mm (Specification of design)
Speed rotation, N: 200rpm (Based onspecification of motor)
Angular velocity: $\frac{2 \pi N}{60}=20.9462(\mathrm{rad} / \mathrm{sec})$
$\mathrm{Ma}=$ mass crank + mass rod $=0.337 \mathrm{~kg}$
$\mathrm{Mb}=2($ mass slider $)+$ mass grip $=1 \mathrm{~kg}$

### 4.2.2 Force Analysis

Force analysis had been made on crank and pins. Force was calculated to define on each angle. Table 4.3 shows the result of calculation for each angle on crank. The calculation will be related to mass, radius, length, and angular velocity to define force for each angle. Furthermore, the result will be located on graph such on Figure 4.2. Force is calculated as on Equation 4.2.

$$
\begin{equation*}
F x=-M a\left(R \omega^{2} \cos (\theta)\right)-M b\left[R \omega^{2}\left(\cos (\theta)+\frac{\mathrm{R}}{\mathrm{~L}} \cos (2 \theta)\right)\right] \tag{4.2}
\end{equation*}
$$



Figure 4.2: X-component, force acting on crank for each angle.
Table 4.3: Result of force acting on crank.

| Angle | Radian | Angula <br> r <br> velocity | Radius(in <br> $)$ | Length(in <br> ) | Mass <br> $\mathrm{kg} \mathrm{(a)}$ | Mass <br> $\mathrm{kg}(\mathrm{b})$ | Force |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | 0 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | -394.596 |
| 20 | 0.3491 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | -362.371 |
| 40 | 0.6982 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | -273.526 |
| 60 | 1.0473 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | -148.759 |
| 80 | 1.3964 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | -14.4709 |
| 100 | 1.7456 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | 105.7335 |
| 120 | 2.0947 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | 197.3566 |
| 140 | 2.4438 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | 256.7557 |
| 160 | 2.7929 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | 288.1136 |
| 180 | 3.142 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | 297.6225 |
| 200 | 3.4911 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | 288.0679 |
| 220 | 3.8402 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | 256.6522 |
| 240 | 4.1893 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | 197.1808 |
| 260 | 4.5384 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | 105.4828 |
| 280 | 4.8876 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | -14.7756 |
| 300 | 5.2367 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | -149.072 |
| 320 | 5.5858 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | -273.785 |
| 340 | 5.9349 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | -362.518 |
| 360 | 6.284 | 20.947 | 0.59 | 3.15 | 0.337 | 1 | -394.596 |

Based on result, the minimum value is -394.596 N which start with 0 degree while the maximum value is 297.6225 N on 180 degree. Table 4.4 shows the result of calculation for displacement for each angle on crank. Furthermore, the result of displacement will be plot on graph such on Figure 4.3. Displacement will be defined as distance of gripper on slider when were pulled or push. Calculation will be related to radius and length of part design. Force will be calculated as on Equation 4.3.

$$
\begin{equation*}
S(\theta)=L-\frac{R^{2}}{4 L}+R\left[\sin (\theta)+\frac{R}{4 L}(\sin (2 \theta)]\right. \tag{4.3}
\end{equation*}
$$



Figure 4.3: X-component, displacement between slider.

Table 4.4: Result of displacement between slider.

| Angle | Radian | Angular <br> velocity | Radius | Length | Displacement | Stroke(mm) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | 0 | 20.947 | 15 | 80 | 79.297 | 8.203125 |
| 20 | 0.3491 | 20.947 | 15 | 80 | 84.88 | 2.620176 |
| 40 | 0.6982 | 20.947 | 15 | 80 | 89.632 | -2.13219 |
| 60 | 1.0473 | 20.947 | 15 | 80 | 92.897 | -5.3971 |
| 80 | 1.3964 | 20.947 | 15 | 80 | 94.31 | -6.80971 |
| 100 | 1.7456 | 20.947 | 15 | 80 | 93.828 | -6.32762 |


| 120 | 2.0947 | 20.947 | 15 | 80 | 91.676 | -4.1761 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 140 | 2.4438 | 20.947 | 15 | 80 | 88.243 | -0.74268 |
| 160 | 2.7929 | 20.947 | 15 | 80 | 83.971 | 3.529497 |
| 180 | 3.142 | 20.947 | 15 | 80 | 79.291 | 8.208662 |
| 200 | 3.4911 | 20.947 | 15 | 80 | 74.613 | 12.88736 |
| 220 | 3.8402 | 20.947 | 15 | 80 | 70.342 | 17.15809 |
| 240 | 4.1893 | 20.947 | 15 | 80 | 66.911 | 20.58904 |
| 260 | 4.5384 | 20.947 | 15 | 80 | 64.763 | 22.73707 |
| 280 | 4.8876 | 20.947 | 15 | 80 | 64.285 | 23.21491 |
| 300 | 5.2367 | 20.947 | 15 | 80 | 65.702 | 21.79781 |
| 320 | 5.5858 | 20.947 | 15 | 80 | 68.971 | 18.52888 |
| 340 | 5.9349 | 20.947 | 15 | 80 | 73.726 | 13.77371 |
| 360 | 6.284 | 20.947 | 15 | 80 | 79.31 | 8.189759 |

Based on result, the minimum value on displacement graph is 64.285 mm and the maximum value is 94.31 mm . The maximum value show the highest distance of gripper on slider when pulled. In addition, acceleration also can be defined by a calculation such on Table 4.5. Result will be identified based on graph such on Figure 4.4. Slider acceleration will be calculated on Equation 4.4.

$$
\begin{equation*}
A(\theta)=\left[-R \omega^{2}\left(\sin (\theta)+\frac{R}{L} \cos (2 \theta)\right)\right] \tag{4.4}
\end{equation*}
$$

Table 4.5: Result of acceleration on slider.

© \begin{tabular}{r|r|r|r|r|r|}

Angle \& \multicolumn{1}{c|}{ Radian } \& | Angular |
| :---: |
| velocity | \& Radius \& Length \& Acceleration <br>

\hline 0 \& 0 \& 20.947 \& 15 \& 80 \& 0 <br>
\hline 20 \& 0.3491 \& 20.947 \& 15 \& 80 \& -3044.56 <br>
\hline 40 \& 0.6982 \& 20.947 \& 15 \& 80 \& -5446.24 <br>
\hline 60 \& 1.0473 \& 20.947 \& 15 \& 80 \& -6768.67 <br>
\hline 80 \& 1.3964 \& 20.947 \& 15 \& 80 \& -6903.3 <br>
\hline 100 \& 1.7456 \& 20.947 \& 15 \& 80 \& -6058.61 <br>
\hline 120 \& 2.0947 \& 20.947 \& 15 \& 80 \& -4629.77 <br>
\hline 140 \& 2.4438 \& 20.947 \& 15 \& 80 \& -3013.74 <br>
\hline 160 \& 2.7929 \& 20.947 \& 15 \& 80 \& -1456.22 <br>
\hline 180 \& 3.142 \& 20.947 \& 15 \& 80 \& 1.675579 <br>
\hline 200 \& 3.4911 \& 20.947 \& 15 \& 80 \& 1459.716 <br>
\hline
\end{tabular}

| 220 | 3.8402 | 20.947 | 15 | 80 | 3017.494 |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 240 | 4.1893 | 20.947 | 15 | 80 | 4633.461 |
| 260 | 4.5384 | 20.947 | 15 | 80 | 6061.432 |
| 280 | 4.8876 | 20.947 | 15 | 80 | 6904.259 |
| 300 | 5.2367 | 20.947 | 15 | 80 | 6766.991 |
| 320 | 5.5858 | 20.947 | 15 | 80 | 5441.779 |
| 340 | 5.9349 | 20.947 | 15 | 80 | 3037.984 |
| 360 | 6.284 | 20.947 | 15 | 80 | -7.37255 |



Figure 4.4: X-component, accelerationon slider.

Table•4.6 shows the result for the velocity of motor while it rotates. The result will be plot on graph such on Figure 4.5 which to know the minimum value and maximum value of velocity on each angle. Based on result velocity, the value will be referring on Equation 4.5

$$
\begin{equation*}
\mathrm{V}(\theta)=\omega \mathrm{R}\left[\cos (\theta)+\frac{\mathrm{R}}{2 \mathrm{~L}} \cos (2 \theta)\right] \tag{4.5}
\end{equation*}
$$



Figure 4.5: X-component, velocity of slider.
Table 4.6: Result of Slider Velocity.

| Angle | Radian | Angular <br> velocity | radius | Velocity <br> $(\mathrm{mm} / \mathrm{sec})$ |  |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 0 | 0 | 20.947 | 15 | 80 | 343.6563 |
| 20 | 0.3491 | 20.947 | 15 | 80 | 317.8096 |
| 40 | 0.6982 | 20.947 | 15 | 80 | 245.7827 |
| 60 | 1.0473 | 20.947 | 15 | 80 | 142.328 |
| 80 | 1.3964 | 20.947 | 15 | 80 | 26.82077 |
| 100 | 1.7456 | 20.947 | 15 | 80 | -82.3055 |
| 120 | 2.0947 | 20.947 | 15 | 80 | -171.888 |
| $140^{\circ}$ | 2.4438 | 20.947 | 15 | 80 | -235.622 |
| 160 | 2.7929 | 20.947 | 15 | 80 | -272.712 |
| 6180 | 3.142 | 20.947 | 15 | 80 | -284.744 |
| 200 | 3.4911 | 20.947 | 15 | 80 | -272.655 |
| 220 | 3.8402 | 20.947 | 15 | 80 | -235.504 |
| 240 | 4.1893 | 20.947 | 15 | 80 | -171.708 |
| 260 | 4.5384 | 20.947 | 15 | 80 | -82.0698 |
| 280 | 4.8876 | 20.947 | 15 | 80 | 27.08928 |
| 300 | 5.2367 | 20.947 | 15 | 80 | 142.5912 |
| 320 | 5.5858 | 20.947 | 15 | 80 | 245.9944 |
| 340 | 5.9349 | 20.947 | 15 | 80 | 317.9279 |
| 360 | 6.284 | 20.947 | 15 | 80 | 343.6561 |

4.3 Analysis using CATIA software

Analytical analysis is done to evaluate the strength of material based on yield strength and Von Misses value. There are two parts that had been analyzed which is pin and crank. Force that will apply on both parts is 613.33 N based on Equation 4.5 that had been figured. Two of parts will be generated on structural analysis to define their load and constraints to perform a computation.

$$
\begin{equation*}
\text { Force }=\frac{\text { Torque }}{\text { Radius }} \tag{4.5}
\end{equation*}
$$

Before analyze the material need to be chosen to applyon structural design. There is general process for static analysis which is from define material, apply restraints, apply load, perform computation, create images, analyze the result, and lastly refine the analysis. Furthermore, meshing is important part where to determine the result of calculations based on its size and type. The smaller value of size, the result will be better and take long time to simulate. Figure 4.6 shows there are twotypes of meshing which is linear and parabolic. The different between linear and parabolic is parabolic is more accurately than linear because of number of nodes such on Figure 4.7.


Figure 4.6: Octree Tetrahedron.


Figure 4.7: Linear Tetra and Parabolic Tetra.

### 4.3.1 Crank analysis

Maximum stress need to be defined from analysis to compared yield strength of material and know the strength of material start to deform or not. There is several type of structural analysis that had been defined which is deformed mesh; von misses stress, displacement, stress principal andestimated local error. All of this has different of their structural surface. Table 4.7 will show type of material that had been analyzed based on steel material.

Table 4.7: Material of Crank.

| Material | Steel |
| :--- | :--- |
| Young Modulus | $2 \mathrm{e}+011 \mathrm{~N} / \mathrm{m}^{2}$ |
| Poisson Ratio | 0.266 |
| Density | $7860 \mathrm{~kg} / \mathrm{m}^{3}$ |
| Thermal Expansion | $1.17 \mathrm{e}-005 / \mathrm{Kdeg}$ |
| Yield Strength | $2.5 \mathrm{e}+008 \mathrm{~N} / \mathrm{m}^{2}$ |

Table 4.8: Factor of Safety.

| Von Misses Stress | Yield strength | FOS |
| :--- | :--- | :--- |
| $8.47 \mathrm{e}+006 \mathrm{~N} / \mathrm{m}^{2}$ | $2.5 \mathrm{e}+008 \mathrm{~N} / \mathrm{m}^{2}$ | 29.5 |

Deform mesh will be displayed about no of nodes and element that had been applied on structural design such as Figure 4.8. For Von Misses stress, the maximum value had been figured which are $8.47 \mathrm{e}+006 \mathrm{~N} / \mathrm{m}^{2}$ such as Figure 4.9. Based on this, value of Von Misses stress will be compared with yield strength to know the design is failure or not. From result, value of Von misses stress is lower than yield strength which means the design will be not failure such on Table 4.8.


Figure 4.8: Deformed Mesh.


Figure 4.9: Von Misses Stress.

Table 4.9 shows the position ofmaximum stress value that had been analyzed.The red color show on displacement, stress principal, and estimated local error which mean it is the maximum stress value. Redcolor means the maximum value of stress that was applied on that area. Each of structural analysis will be given different minimum and maximum value. Moreover, displacement, stress principal, and estimated local error will show different type structure of force.

Table 4.9: Structural Analysis of Crank.

| Analysis | Description |
| :--- | :--- |




### 4.3.2 Crank Improvement Analysis

After analyzed crank, value of Von Misses stress had been decreased than before while improves it. Size of crank need to be redesign to make more strength and long lifespan while use it. Thickness of crank had been change from 5 mm to 7 mm and diameter of pin from 8 mm to 10 mm as shown in Figure 4.10.


Figure 4.10: Crank.

The result was compared with Von Misses value from before and after. Based on this, thickness effected on result while improve it and the value of Von Misses stress became decreased than before. Table 4.10 shows the different value of Von Misses stress before and after analyzed for both. In addition, the design will be failed if the maximum value of Von Misses stress reaches at critical point or yield point for ductile material or the maximum value of VongMisses stress more than it strength. Figure 4.11 shows the maximum value of Voñ Misses stress at certain area.

Table 4.10: Von Misses Stress Value.

| Before | After |
| :--- | :--- |
| $8.47 \mathrm{e}+006 \mathrm{~N} / \mathrm{m}^{2}$ | $3.86 \mathrm{e}+006 \mathrm{~N} / \mathrm{m}^{2}$ |



Figure 4.11: Von Misses Stress.

### 4.3.3 Pin analysis

Other than that, for second analysis is made on two pins with same size and area. There are on middle of crank and other one at middle of gripper. Pin will be analyzed to find strength and-matterial that suitable. Steel had been applied on pinfor analyzed with several type of structure analysis which is deformed meshed, Von Misses stress, displacement, principal stress, and estimated error. Table 4.11 will show material steel that had been analyzed based on application material. Furthermore, the result factor of safety is shownin Table 4.12.

Table 4.11: Material of Pin.

| Material | Steel |
| :--- | :--- |
| Young Modulus | $2 \mathrm{e}+011 \mathrm{~N} / \mathrm{m}^{2}$ |
| Poisson Ratio | 0.266 |


| Density | $7860 \mathrm{~kg} / \mathrm{m}^{3}$ |
| :--- | :--- |
| Thermal Expansion | $1.17 \mathrm{e}-005 / \mathrm{Kdeg}$ |
| Yield Strength | $2.5 \mathrm{e}+008 \mathrm{~N} / \mathrm{m}^{2}$ |

Table 4.12: Factor of Safety.

| Von Misses Stress | Yield strength | FOS |
| :--- | :--- | :--- |
| $6.92 \mathrm{e}+006 \mathrm{~N} / \mathrm{m}^{2}$ | $2.5 \mathrm{e}+008 \mathrm{~N} / \mathrm{m}^{2}$ | 36.1 |

Based on figure 4.12, nodes and element had been applied on deformed mesh analysis. Based on result, the maximum value of Von.Misses stress that had been figure is $6.92 \mathrm{e}+006 \mathrm{~N} / \mathrm{m}^{2}$ such on Figure 4.13 . The value still lower than yield strength and the design cannot failure.


Figure 4.12: Deformed Mesh.


Figure 4.13: Von Misses Stress.

Table 4.13shows the position of maximum stress value that had been analyzed. The maximum stress value shows on red color as before. Each of structural analysis will be given different minimum and màximum value. In addition, displacement, stress principal, and estimated local error willshow different type structure of force.

Table 4.13: Structural Analysis of Pin.

| Analysis |  | Description |
| :--- | :--- | :--- |
| Displacement |  |  |


| Stress Principal | Minimum value:-7.48136e+006N/m² |
| :--- | :--- | :--- |
| Maximum value: 1.5874e+006N/m² |  |
| Estimated Local Error | Minimum value:3.94867e-014J |
| Maximum value: 1.60029e-007J |  |
| Estimated Precision: 4.05558e-006J |  |
| Strain Energy: 7.58795e-006J |  |
| Global estimated error: 45.9219 \% |  |

4.3.4 Pin Improvement Analysis

Diameter of the pin had been change from 8 mm to 10 mm to improve the strength of pin and long life span. Based on result, maximum value of Von Misses stress had been decreased when improves the thickness or diameter of pin. Figure 4.14 shows the thickness of pin had been change from before.


Figure 4.14: Pin.

After improve it, the result will be compared with Von Misses value before. The comparison will show on Table 4.14 and the value became decrease than before after improve it. The thickness will affected on resultif improve it where the design will be not fail if maximum value of Von Misses stress not reach at yield point. Figure 4.15 shows critical area on pin that had been analyzed.

Table 4.14: Von Misses Stress Value.

| Before | After |
| :--- | :--- |
| $6.92 \mathrm{e}+006 \mathrm{~N} / \mathrm{m}^{2}$ | $3.36 \mathrm{e}+006 \mathrm{~N} / \mathrm{m}^{2}$ |



Figure 4.15: Von Misses stress.

### 4.4 Product Costing

Product costing related to the managing of account or serve management on design product. It will be related to the fixed cost and variable cost. Fixed cost explained about tool or equipment that on fabrication product where variable cost is item or part of component that were used on designing product. Manufacturing cost defined as total cost for overalf to selling the product. Table 4.15shows type of component part design for estimating cost of one product.

Table 4.15: Part Design.

| Item | Quantity | Cost Per Unit <br> (RM) | Total Cost (RM) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Slider | 2 | RM450.00 | Rm900 |  |  |
| Motor | 1 | RM231.98 | Rm231.98 |  |  |
| Bearing | 1 | RM67.83 | RM67.83 |  |  |
| Shaft | 1 | RM15.00 | RM15.00 |  |  |
| Round plate | 2 | RM23.97 | Rm47.94 |  |  |
| Rod steel | 1 | RM15.00 | RM15.00 |  |  |
| Steel square tube | 1 | RM40.00 | Rm40.00 |  |  |
| Zinc | 1 | Rm40.00 | Rm40.00 |  |  |
| Total |  |  |  |  | RM1357.75 |

### 4.5 Summary

Analysis and simulation on design product had been achieved on the result by using CATIA software. Based on analysis, using of steel material cannot failure because the maximum of value Von Misses still not exceed on yield strength of material. The analysis had been figure on crank and pin. For the simulation, bell shape graph had been form based on proven theoretically calculation. The calculation had been identified by force, angular velocity, and•mass of part design to form a graph. For overall, fatigue tensile will be form based on simulation and analysis that had been identified.


[^0]:    | Motion of gripper | Description |
    | :--- | :--- |

